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Antoine Le Duigou, Peter Davies, Christophe Baley. Macroscopic Analysis of Interfacial properties of Flax/PLLA biocomposites. Composites Science and Technology, 2010, 70 (11), pp.1612. 10.1016/j.compscitech.2010.06.001 . hal-00666484

HAL Id: hal-00666484

<https://hal.science/hal-00666484>

Submitted on 5 Feb 2012

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Accepted Manuscript

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PII: S0266-3538(10)00227-7
DOI: [10.1016/j.compscitech.2010.06.001](https://doi.org/10.1016/j.compscitech.2010.06.001)
Reference: CSTE 4736

To appear in: *Composites Science and Technology*

Received Date: 19 December 2009
Revised Date: 31 May 2010
Accepted Date: 2 June 2010



Please cite this article as: Le Duigou, A., Davies, P., Baley, C., Macroscopic Analysis of Interfacial properties of Flax/PLLA biocomposites, *Composites Science and Technology* (2010), doi: [10.1016/j.compscitech.2010.06.001](https://doi.org/10.1016/j.compscitech.2010.06.001)

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Macroscopic Analysis of Interfacial properties of Flax/PLLA biocomposites

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Abstract :

This study presents results from a study of the mechanical behaviour of flax reinforced Poly(L-Lactic Acid) (PLLA) under in-plane shear and mode I interlaminar fracture testing. Slow cooling of the unreinforced polymer has been shown to develop crystalline structure, causing improvement in matrix strength and modulus but a drop in toughness. The in-plane shear properties of the composite also drop for the slowest cooling rate, the best combination of in-plane shear performance and delamination resistance is noted for an intermediate cooling rate, (15.5°C/min). The values of G_{Ic} obtained at this cooling rate are higher than those for equivalent glass/polyester composites. These macro-scale results have been correlated with microdroplet interface debonding and matrix characterization measurements from a previous study. The composite performance is dominated by the matrix rather than the interface.

Keywords : A. Fibres, A. Polymer matrix composites (PMCs), B. Interface, B. Interfacial strength, B. Delamination

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1 Introduction

The development of composite materials for large scale industrial applications, such as those in which glass reinforced polyester is currently employed, raises a number of environmental questions, particularly regarding end-of-life management. An increasing demand for materials which respect the environment has encouraged research into alternatives which are not based on fossil fuels and have a low global warming impact. One solution is to develop biocomposites such as flax fibre reinforced Poly(L-Lactic Acid) (PLLA). This type of material is recyclable [1] and bio-degradable by composting. In addition, the analysis of environmental impacts, evaluated from raw material extraction through to end of life, has shown that compared to glass/polyester composites their non-renewable energy consumption is divided by two. Different impacts such as global warming are also significantly reduced, though a transfer of pollution occurs towards eutrophication [2]. The quasi static tensile modulus values of biocomposites are satisfactory [1, 3] but their failure stresses are lower than those of glass/polyester composites. At the micro-mechanics scale Le Duigou et al [4], using a micro-droplet test to measure Interfacial Shear Strength on flax/PLLA, showed good interface properties, comparable to those of a glass/polyester combination. The strength of the flax/PLLA interface is influenced by the morphology of the semi-crystalline PLLA matrix and by residual thermal stresses induced by thermal treatments [4].

However, in order to study the influence of interface behaviour on the mechanical properties of laminated composites a change of scale is necessary. A certain number of mechanical tests are often used to evaluate the macroscopic interface strength of composites [5]. Among these are transverse tensile, in-plane shear by tension on a $\pm 45^\circ$ laminate, short beam interlaminar shear, and interlaminar fracture tests. Few of these have been applied to biocomposites. Baley et al. [6] measured transverse tensile properties of flax/polyester composites. Their transverse strength was similar to that of glass/polyester composites (respectively 13 ± 0.6 MPa compared to 15 ± 2.5 MPa). Rohmany et al [7] used the tensile test on $\pm 45^\circ$ Materbi/flax biocomposite laminates. However, they presented their results in terms of tensile rather than in-plane shear properties as the transverse strain was not measured. There is very little data available on either interlaminar or intralaminar shear strength of biocomposites. Concerning interlaminar fracture, mode I tests on glass mat/PLLA biocomposite indicated a low G_{Ic} value of 39 ± 8 J/m² [8]. For comparison, the mode I fracture toughness G_{Ic} of a unidirectional glass reinforced Polyester is around 90 J/m² [9]. Davies et al [10] and Perrin et al. [11] have shown how the microstructure of a semi-

crystalline polymer matrix affects the delamination resistance of glass/PP composites. According to the cooling rate after moulding the G_{Ic} value for the composite varies from 220 J/m² to 1270 J/m². Faster cooling resulted in improved fracture energies. Herrera-Franco et al [5] compared fibre-matrix adhesion measurements for carbon/epoxy with and without a fibre sizing, both at the micro scale (microdroplet debonding, fragmentation...) and the macro scale (tension $\pm 45^\circ$, Iosipescu, short beam shear...). Their study indicated similar trends for the influence of sizing at the two scales. Nevertheless some differences were seen, in particular due to the assumptions used in the calculations [5].

The aim of the present study is to evaluate the behaviour of flax/PLLA under in-plane shear and mode I delamination as a function of the parameters which influence fibre/matrix adhesion; these were previously shown in [4] to be the degree of crystallinity, the morphology of the matrix, and residual stresses. A comparison with results from the previous study, performed on the same fibres and matrix, will be made.

2 Materials and methods

2.1 Specimen manufacture

Specimens for in-plane shear were prepared according to ASTM D3518 [12] with PLLA reinforced by ($\pm 45^\circ$) flax layers. Fibre weight content is around 30%. The biopolymer is a thermoplastic Poly(L-lactic acid) or PLLA reference L9000 from Biomer®. The fibres were supplied, in the form of layers of two unidirectional tapes of untwisted yarns in a 0/90° configuration, stitched together with cotton thread, by C.R.S.T (France) with an areal weight of 500g/m². The fibres were grown in France and had been dew retted before stripping and combing. The shear test standard requires a $[45/-45]_{ns}$ stacking sequence with $2 < n < 4$, and at least 8 reinforcement layers to limit tension-flexion coupling [13] and increase the interlaminar area. Specimens were rectangular with the following dimensions : (25x160x6.5) mm³. They were prepared using the cycle shown in figure 1. Four conditions were examined; three different cooling cycles were applied, as shown in figure 2, plus an anneal below the glass transition temperature (T_g). Cooling rates were measured by insertion of thermocouples at mid-thickness of the samples. Figure 2 shows measured values, with an almost linear cooling rate for slow cooling (A), the difference between the set moulding machine temperature and the specimen is small. At faster cooling rates the measured temperature is hyperbolic with a rapid drop to around 100°C followed by a slower drop to room temperature.

This shape can be explained by the thermal inertia of the material. The cooling rates presented subsequently are estimated using the slopes of the curves over the range of temperatures in which the polymer morphology and the residual stresses are strongly influenced by cooling rate. For semi-crystalline samples, this range is between T_{\max} and melting temperature T_f . For the amorphous samples it is between T_{\max} and T_g . The values of these temperatures were measured initially using DSC (Differential Scanning Calorimetry).

These three cooling rates were applied in order to obtain different morphologies in the PLLA matrix. An anneal for 72 h below T_g at 50°C enables residual stresses, generated by rapid cooling (quench in water) to be released without developing crystalline structure. The annealing time is determined using DSC. An endothermic peak appears at T_g corresponding to the delayed reorganisation necessary to reach equilibrium.

The procedure to produce specimens for delamination resistance tests was similar to that described above, but with a shorter time at 190°C (Fig. 1) as the thickness is less (4mm compared to 6.5 mm). The fibre content is the same, but here the biocomposite tested is reinforced by flax in the form of mat. The ISO 15024 [14] standard is applied, although it is primarily intended for testing delamination of unidirectionally reinforced composites. The flax mat is produced using a paper-making route. This results in a quasi-isotropic in-plane fibre distribution which is interesting as it minimizes the weaknesses of natural fibres, their poor transverse and shear properties [15]. The mat also allows fibres with 9 ± 1 mm length and a high aspect ratio ($L/d \approx 470$) to be used, as fibre bundles are separated during the mat production process. The mats used here have an areal weight around 150g/m² and have not undergone any chemical or physical surface treatment.

A Teflon film 20 microns thick is inserted at mid-thickness during manufacture to provide a starter crack. This is slightly thicker than the ISO 15024 [14] standard recommends (<13 microns). It is also not possible to measure G_{Ic} values on these mat reinforced composites directly as their flexural properties are too low, so they are bonded to machined aluminium reinforcements of dimensions (200x20x4) mm³ (Fig. 4). Ten specimens with different initial starter crack lengths a_0 ($40 < a_0 < 75$ mm) were tested for each material.

2.2 Mechanical tests

2.2.1 Tension $\pm 45^\circ$: In-plane shear

The in-plane shear specimens underwent similar thermal treatments to those applied to microdroplets previously [4] in order to be able to compare results. This tensile test on \pm

45° laminates was chosen as it is sensitive to interface and matrix properties. Tests were performed according to ASTM D 3518 [12] on an Instron 8803 machine with a 50kN load cell, at a crosshead displacement rate of 2 mm/min. An MTS biaxial extensometer was used to measure longitudinal and transverse strains. This test provides shear stress τ_{12} , shear strain γ_{12} and shear modulus G_{12} values. Modulus G_{12} was determined from the slope of the plot of shear stress Eq. (1) versus shear strain (equation 2) in the range γ_{12} range between 0 and 0.2%.

$$\tau_{12} = \frac{\sigma_x}{2} \quad (1)$$

where σ_x is the applied stress.

$$\gamma_{12} = (\epsilon_x^0 - \epsilon_y^0) \quad (2)$$

Particular attention is required for stress values. A 1° fibre rotation occurs for an axial strain of 2 %. According to the ASTM D3518 standard [12] if the shear strain is below 5% the shear stress can be taken as the maximum value ($\sigma_x = \sigma_{\max}$), if not then the value at $\gamma = 5\%$ should be used and $\sigma_x = \sigma_{5\%}$.

The limitations of the test are :

- A lack of accuracy in strain measurements due to material heterogeneity, with resin rich regions and stitching fibres.
- The shear stress state in the sample, which is not pure due to interlaminar shear and normal stresses [5].
- Fibre angle variability.

For the unreinforced matrix shear properties were calculated from tensile data assuming isotropic behaviour and a Von Mises criterion:

$$G_{12} = \frac{E}{2(1 + \nu)} \quad (3)$$

$$\tau_{12} = \frac{\sigma}{\sqrt{3}} \quad (4)$$

The shear modulus G_{12} of a unidirectional composite may be estimated using the Halpin-Tsai equation [16] :

$$\frac{M}{M_m} = \frac{1 + \xi \cdot \eta \cdot V_f}{1 - \eta \cdot V_f} \quad (5)$$

with

$$\eta = \frac{\frac{M_f}{M_m} - 1}{\frac{M_f}{M_m} + \xi} \quad (6)$$

where $M = G_{LT}$, $M_f = G_f$, $M_m = G_m$. m, f, L and T indicate respectively the matrix, the fibre, and longitudinal and transverse properties. V_f is the fibre volume fraction and ξ a form factor which depends on the geometry of the fibre and loading type. $\xi = 1$ here [16] with an L/d ratio of 470. The value of G_{fT} is taken to be 3315 MPa, based on previous work by Baley et al on flax fibres [17]. It should be emphasized that the aim here is not to develop a micro-mechanics analysis, but simply to compare measured shear modulus values with those estimated using a simple expression which is widely-used on traditional glass and carbon reinforced materials.

2.2.2 Mode I delamination

The mode I delamination test, which enables the critical strain energy release rate G_{Ic} to be measured, was chosen as it is also sensitive to interface and matrix properties. The Double Cantilever Beam (DCB) specimen (Fig. 3a) allows the energy required to initiate and propagate a crack from a thin film defect to be quantified. Here only the initiation values will be discussed, as described by the ISO 15024 standard [14], subsequent propagation values are controversial as the crack can wander through the mat thickness and multiple cracks may be generated [18, 19]. Various techniques can be used to detect crack initiation, including the non-linearity of the load-displacement plot, acoustic emission, strain gauge recording slope changes, and visual or camera observation [20]. Here, observation using a Sony digital camera was employed, linked to an in-house data acquisition system which also records images, together with the load (F) and opening displacement () from an MTS RT 1000 test machine, at 2 Hz. (Fig. 3b). White paint on the specimen edge helps to reveal the crack (Fig. 3c). Loading rate was 2 mm/minute.

The value of G_{Ic} corresponding to initiation was determined using a compliance calibration approach:

$$G_{Ic} = \frac{F^2}{2b} \frac{dC}{da} \quad (7)$$

where C is the compliance:

$$C = \frac{\delta}{F} \quad (8)$$

The compliance calibration used here is that proposed by Berry [21]:

$$C = ka^n \quad (9)$$

where the value of n is determined experimentally by plotting $\ln(C)$ versus $\ln(a)$. k is a constant. Here different initial crack lengths were used to establish this relationship.

The value of strain energy release rate G_I can then be obtained as :

$$G_I = \frac{nF\delta}{2ba} \quad (10)$$

where b is the specimen width. A critical G_{Ic} initiation value is then calculated from the load value at observed initiation.

2.2.3 Matrix fracture toughness

A notched three point flexure test was used to determine the matrix fracture toughness [22] (ISO 13586). The specimens were rectangular, of thickness, B (4mm), and width W with an initial crack length a. The specimens respect the size imposed by the standard:

$4B > W > 2B$, $L = 4W$, $0.45 < a/W < 0.55$, and all dimensions $> 2.5 (K_{Ic}/\sigma_y)^2$.

The notch is introduced by a saw cut followed by tapping a new razor blade to precrack it. This is not a trivial operation with a brittle polymer and there is a tendency to produce shorter cracks which results in an overestimation of K_{Ic} and G_{Ic} .

Loading rate is 10 mm/min to limit crack tip blunting. A critical stress intensity factor K_{Ic} is calculated as [23]:

$$K_{Ic} = \frac{3LF_{\max}}{BW^2} \left(\frac{\pi W}{2} \right)^{0.5} \quad (11)$$

where F_{\max} is the maximum force, L the distance between supports, B and W are respectively the width and thickness of the specimens. A fracture energy G_{Ic} can be determined from K_{Ic} using the expression :

$$G_{Ic} = \frac{K_{Ic}^2}{E} (1 - \nu^2) \quad (12)$$

with E Young's modulus and ν the Poisson's ratio.

Samples were made using the same procedure as for the composites, with the same thermal treatments.

2.2.4 DSC

Thermal analysis was performed using a Mettler Toledo DSC on samples weighing around 10mg. These were first heated at 190°C for 3 minutes to measure melting enthalpies.

Crystallization enthalpies were also measured during heating, by integrating over a fixed temperature range. The degree of crystallinity (χ_c) was estimated using Eq. (13) :

$$\chi_c = (\Delta H_m - \Delta H_c) / \Delta H_{100\%} \quad (13)$$

with $\Delta H_{100\% \text{ crystalline}} = 93.7 \text{ J/g}$ [24].

2.2.5 Scanning Electron Microscopy (SEM)

Fracture surfaces, coated with a thin gold layer, were examined in a Jeol JSM 6460LV SEM.

2.2.6 Polarization microscopy

As PLLA is a semi-crystalline polymer, crystallization can occur during cooling. Thin films were prepared, by hot compression, and observed under an optical polarized light microscope on a Mettler Toledo heated stage in order to study the morphology at different cooling rates.

3 Results and discussion

3.1 PLLA matrix properties

3.1.1 Thermal properties

Table 1 shows how different cooling rates and annealing affect the unreinforced matrix structure. Quenching at 93°C/min results in an amorphous PLLA structure, (Table 1), no crystalline structure (spherulites) is visible (Fig. 4a). Annealing at 50°C (below the T_g of 65°C) does not result in a recrystallization. Slower cooling results in an increase in degree of crystallinity, reaching 33%. This is in agreement with previous studies [25] on similar materials. It is interesting to note, however, that the degree of crystallinity is lower than that

found in a previous study of microdroplets of the same polymer [4]. The difference is due to slightly different cooling rates and, above all, to the difference in specimen volume ($V_{\text{microdroplet}} \approx 8.10^{-13} \text{ cm}^3$ compared to $V_{\text{bulk sample}} \approx 10 \text{ cm}^3$). Fig. 4b and c show the appearance of spherulites whose size increases at slower cooling rate ($1.5^\circ\text{C}/\text{min}$). Some inter-spherulitic defects are visible, particularly for samples cooled at $1.5^\circ\text{C}/\text{min}$. These may result in poor bonding between the spherulites [10].

3.1.2 Thermomechanical Properties

Table 2 presents the mean measured tensile properties and their standard deviations and estimated shear properties of the PLLA matrix for the different thermal conditions. The tensile data were presented previously [4]. Slow cooling results in improved modulus and strength, due to higher crystallinity. However, failure strain is reduced. These properties are very similar to those of orthophthalic polyester resins [9] which are commonly used in glass fibre reinforced composites. The low failure strain of PLLA, whatever the cooling cycle, is a weak point and alternative grades with higher failure strains are being evaluated. Faster cooling (15.5 et $93^\circ\text{C}/\text{min}$) results in a small reduction in PLLA properties.

3.1.3 Fracture toughness

Table 3 shows mean critical stress intensity (K_{Ic}), strain energy release rate (G_{Ic}) values and their standard deviations for the PLLA polymer for the different conditions. For the slowest cooling rate ($1.5^\circ\text{C}/\text{min}$), K_{Ic} and G_{Ic} are low, similar to values respectively measured on orthophthalic ($K_{Ic} = 0.419$) [26] and isophthalic polyester resins ($K_{Ic} = 0.45 \text{ MPa.m}^{0.5}$) [26]. The large spherulitic microstructure and in particular the defects between spherulites (Fig. 4c), provide an easier path for crack propagation. Fracture surfaces of specimens cooled at $1.5^\circ\text{C}/\text{min}$ (Fig. 5a) confirm this interspherulitic failure mode. Increasing cooling rate results in a significant increase in K_{Ic} and G_{Ic} for PLLA with values similar to those of some epoxy resins (e.g. $K_{Ic} = 1.125 \text{ MPa.m}^{0.5}$ [26]). The fracture surface for the specimen cooled at $15.5^\circ\text{C}/\text{min}$ is completely different to that of the slower cooled sample (Fig. 5b), plastic deformation is apparent. Quenching reduces K_{Ic} and G_{Ic} slightly, annealing results in a small increase but the differences are small compared to scatter in results. The mechanical properties of the PLLA polymer are controlled by its microstructure in a similar way to those of more conventional polymers.

3.2 Composite in-plane shear

Fig. 6 shows in-plane shear stress-strain plots from tensile tests on $\pm 45^\circ$ laminates of flax/PLLA biocomposite for different thermal conditions. The results are detailed in Table 4. The shear modulus G_{12} of the biocomposites is higher than that of the matrix but shear strength is lower (Table 4). The slow-cooled composite shows extensive surface cracking even before testing (Fig. 7a). There is a difference in thermal expansion coefficients of fibre and matrix (for flax fibre $\alpha_{fL} = -1.10^6 / ^\circ\text{C}$ [27] and for PLLA matrix $\alpha_m = 78.5.10^6 / ^\circ\text{C}$ [4]) but the fibres also limit crystallization shrinkage during spherulite formation. These cracks will limit the load-bearing capacity of the composites but values are still superior to the values for flax/polyester and glass/polyester composites with the same fibre content, V_f 32%, tested previously, $G_{12} = 20.5 \pm 0.8$ and 20.1 ± 1.3 MPa respectively [28].

Composites cooled more quickly do not develop these cracks (Fig. 7b). Fig. 8a shows a fracture surface of a specimen cooled at $1.5^\circ\text{C}/\text{min}$, some interfacial debonding is apparent, with little plastic deformation. As for the PLLA alone the best properties correspond to the intermediate cooling rate ($15.5^\circ\text{C}/\text{min}$). Very fast cooling ($93^\circ\text{C}/\text{min}$) results in lower properties due to lower crystallinity. As shown in Figures 8b and 8c, fracture surfaces of fast cooled specimens indicate interfacial debonding, those of materials cooled at $15.5^\circ\text{C}/\text{min}$ reveal more matrix attached to fibres.

The annealing step has little influence on the behaviour of these biocomposites in shear. The sample size and the annealing time (72h) do not allow significant relaxation [29].

The shear modulus can also be estimated using Eq. (5) and (6). Results are shown in Table 5. The simple model gives a reasonable first estimation of in-plane modulus, overestimating the fast cooled sample values, possibly due to internal stress effects as the annealed material value is closer, and underestimating for the slow cooled specimens.

3.3 Mode I delamination

Mode I delamination tests were performed on flax mat reinforced PLLA. Fig. 9 shows examples of the load-displacement plots for the four sets of materials. Slow cooling ($1.5^\circ\text{C}/\text{min}$) results in lower maximum force and force at non-linearity. The insert in Figure 9 shows all measured initial compliance values versus starter crack length (in meters) on a log-

log plot. An n -value (slope) was determined for each set of samples and used to calculate G_{Ic} with Eq.(9). Values of n were all in the range from 2.1 to 2.6. Table 6 summarizes the results. These values are calculated using the load corresponding to initiation observed visually. The use of the digital camera allows this point to be clearly defined. The results show that apart from the slowest cooled material all these flax/PLLA biocomposites have higher delamination resistance than glass mat reinforced polyester ($\sim 100\text{J/m}^2$) [20], though this comparison should be made with caution as test conditions are not strictly identical (slightly thicker insert here). Concerning the influence of thermal treatments a similar tendency is observed to that noted by Davies et al. [10] and Perrin et al. [11] for UD glass/PP composites cooled at different rates. This can be explained by the reduction in fracture toughness of the slow cooled matrix (Table 2) due to development of crystallinity. The influence of high processing temperature on fibre properties may also play a role [30], this has not been quantified here. Fig. 10a shows mode I fracture surfaces for a slow-cooled specimen. Two mechanisms are apparent. First, residual matrix on the fibre suggests that reasonable fibre-matrix adhesion is possible. Previous work suggested there may be a trans-crystalline phase in this region, though this was not observed [4]. Second, in the right hand photo some traces of fibres can be noted. These are much less marked than for the faster cooling (Fig. 10b, 10c) and show less development of ductile behaviour in the matrix [31]. As for the in-plane shear tests the best results correspond to intermediate cooling rate (15.5°C/min) (Table 6). These combine good matrix fracture toughness, reasonable interface quality [4] and limited internal stresses. The ductile interface (Fig. 10b) suggests strong fibre-matrix interactions [31]. For the fast cooled composite (93°C/min) fibre pull-out and clean fibres indicate early debonding (Fig. 10c). The annealing step has little effect on delamination resistance, once again relaxation is very limited in the reinforced matrix [29], in contrast to the micro-scale samples.

3.4 Micro-Macro relationship, Energy balance.

Damage development during mode I delamination is complex, depending both on matrix properties and fibre/matrix interface behaviour. In a previous study the fracture energy G_{Ic} of the flax fibre/PLLA interface was measured for the same thermal conditions using microdroplet debonding [4]. Based on these data it is possible to propose a delamination energy balance model, using the approach proposed by Dharan et al. [32]. For a UD composite with a hexagonal fibre arrangement and ignoring mode III one obtains :

$$G_{I_{composite}} = 1.05V_f^{0.5}G_{I_{Interface}} + (1 - 1.05V_f^{0.5})G_{I_{matrice}} \quad (14)$$

$$\text{with } V_f = \frac{\pi}{2\sqrt{3}} \left(\frac{d}{h}\right)^2 \quad (15)$$

with d the fibre diameter and h the distance between fibres. However, the reinforcement used here is in mat form, a random in-plane fibre distribution. A square arrangement is therefore used for $G_{I_{composite}}$ of volume:

$$V_f = \frac{\pi}{4} \left(\frac{d}{h}\right)^2 \quad (16)$$

Eq. 14 then becomes :

$$G_{I_{composite}} = 1.13V_f^{0.5}G_{I_{Interface}} + (1 - 1.13V_f^{0.5})G_{I_{matrix}} \quad (17)$$

Table 7 summarizes the results for the strain energy release rates of the PLLA matrix, the flax/PLLA interface and the flax mat/PLLA biocomposite. The results for the biocomposites are compared with estimations made using Eq. (14) and (17). Two fibre arrangements are considered (hexagonal and square) and two loading modes (mode I with or without a mode III component). Cooling rates indicated by an asterisk are those for microdroplet samples. First, it is apparent that fracture energies for matrix, interface and composite are very different (Table 7). Various authors have discussed matrix-composite toughness transfer in the past, notably Hunston [33], who distinguished between brittle matrix resins with fracture energies up to about 200 J/m², for which addition of fibres improved fracture energy, and tougher resins for which fibres reduced the toughness. This was discussed by various authors in terms of constraints on the development of crack tip plastic zones. Here the composite toughness is roughly half that of the matrix. The matrix can dissipate energy through elasto-plastic behaviour but the different tests show that the effects of thermal treatments are not simple. For example, slow cooling (1.5°C/min) increases the fibre-matrix interface toughness but the G_{Ic} of the composite decreases. Annealing does not have a significant effect on mode I delamination resistance (Table 7) nor in-plane shear properties (Table 4) while at the micro scale the relaxation of internal stresses leads to a large drop in interface toughness [4]. At the composite scale the matrix properties and morphology appear to dominate those of the interface. An energy balance approach gives an indication of the trends observed but the notion of a representative volume element to describe a mat layer is open to discussion. Other

phenomena such as friction could also be taken into account in a more complete model. The complex microstructure of the flax fibres may also contribute to cracks propagating within the outer layers of the fibre, indeed Baley et al [6] have indicated cracks developing within the flax fibres in transverse tension tests on flax composites.

4 Conclusion

This study presents results from a study of the behaviour of flax reinforced PLLA under in-plane shear and mode I interlaminar fracture testing. These tests are sensitive to both matrix and interface, and these macro-scale results have been correlated with microdroplet interface debonding and matrix characterization measurements from a previous study.

Flax/PLLA biocomposites with no additional fibre surface treatment show similar in-plane shear properties and mode I delamination resistance values to those of glass/polyester composites. The mechanical properties measured depend strongly on the cooling rate and hence on the matrix microstructure. Slow cooling of the unreinforced polymer has been shown to develop crystalline structure, resulting in an improvement in matrix strength and Young's modulus but a drop in toughness. The in-plane shear properties and G_{Ic} values also drop for the slowest cooling rate. The best combination of in-plane shear performance and delamination resistance is noted for an intermediate cooling rate, (15.5°C/min). These combine good matrix fracture toughness and reasonable interface quality [4]. A simple energy balance approach enables trends in composite fracture energy with cooling rate to be estimated, but the complexity of the natural fibre reinforcement limits quantitative modelling. Current studies are focussed on improving the properties of these materials. Increasing matrix properties, and in particular failure strain is one approach. If further improvements are to be achieved a better understanding of the fibre damage mechanisms is also needed, as the critical element in transverse loading is the cohesion of the fibre itself.

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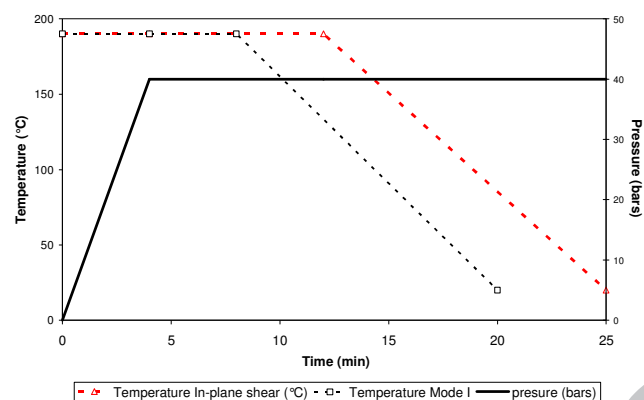


Fig. 1 Film stacking manufacturing cycle for in-plane shear and mode I specimens with water cooling (~ 15.5 °C/min)

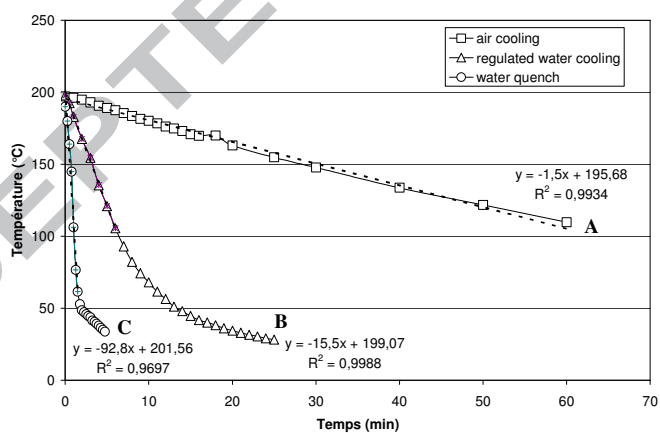


Fig. 2 Cooling kinetics for biocomposites

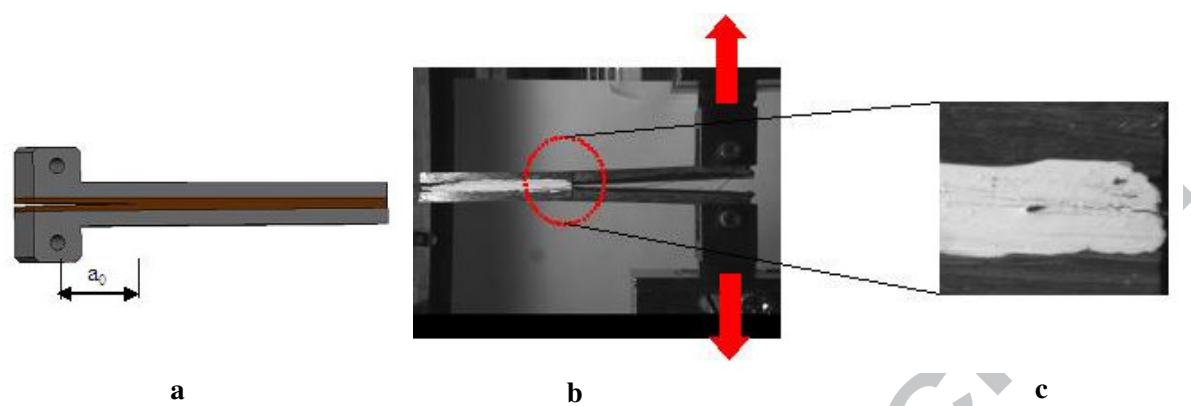


Fig. 3 a). Delamination sample. b)- Delamination test fixture. c)- example of crack tip image recorded

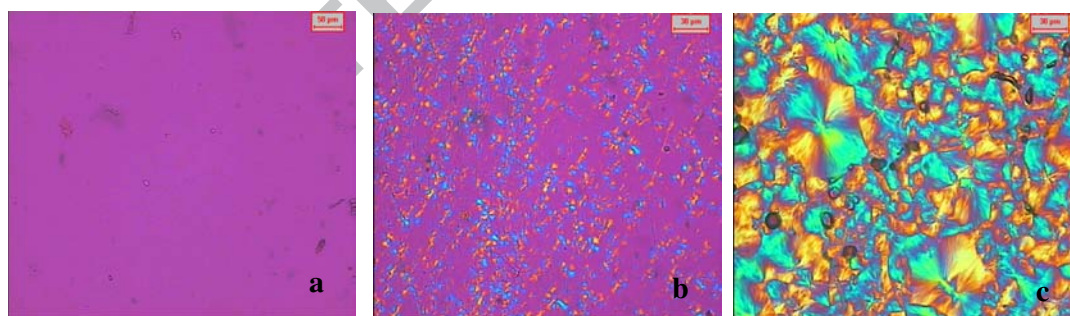


Fig. 4a Matrix morphology of PLLA cooled at 93°C/min. **b** at 15.5°C/min. **c** 1.5°C/min

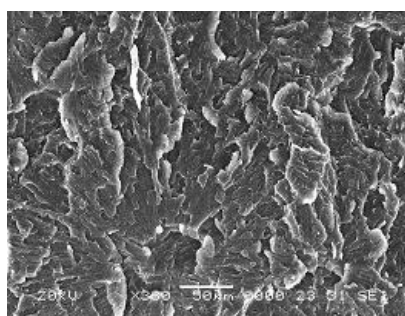
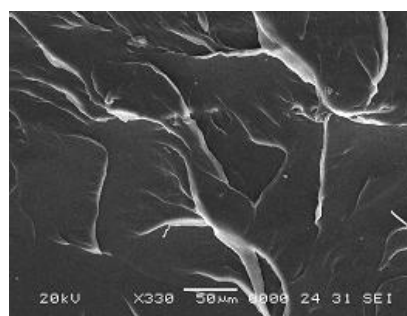
**a****b**

Fig. 5a SEM photography of K_{Ic} specimen fracture surface, 1.5°C/min cooling rate. **b** 15.5°C/min cooling rate

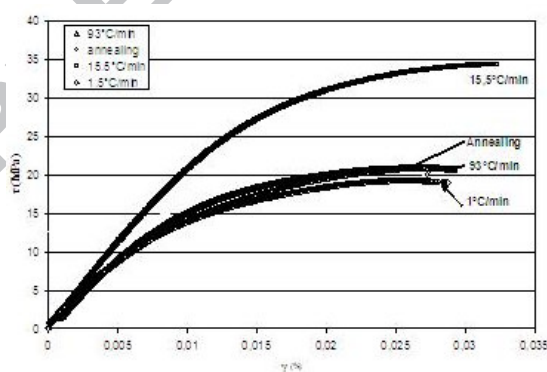


Fig. 6 In-plane shear stress-strain plots

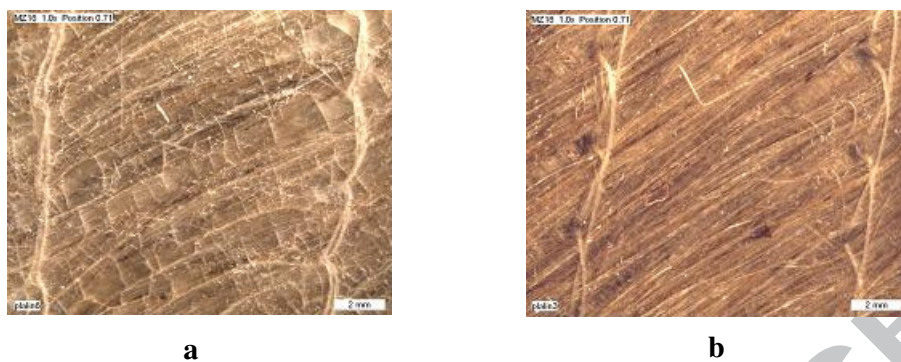


Fig. 7a Surface of biocomposite specimen after cooling at 1.5°C/min. **b.** at 15.5 °C/min

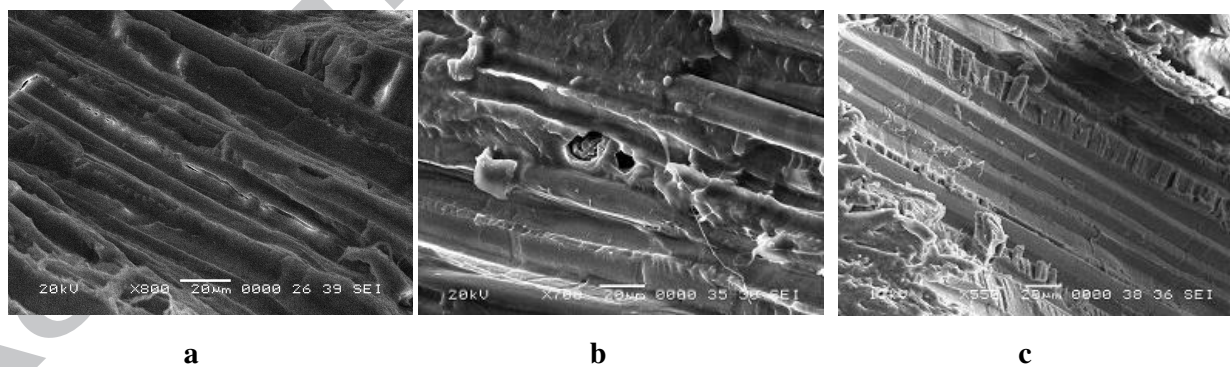


Fig. 8a SEM photography of fracture surface of sample cooled at 1.5°C/min. **b** 15.5°C/min. **c** 93°C/min.

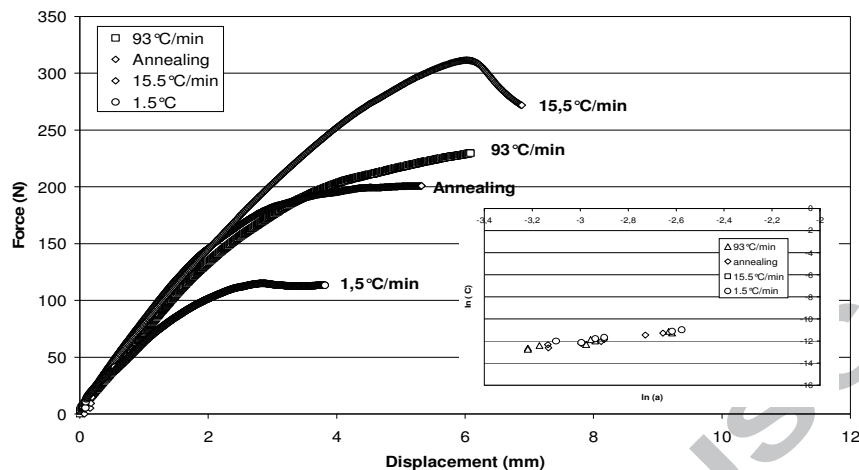


Fig. 9 Force versus opening displacement, mode I, for specimens with $a_0 \approx 70$ mm with different thermal manufacturing conditions. **Insert:** Values of compliance versus initial crack length, all specimens

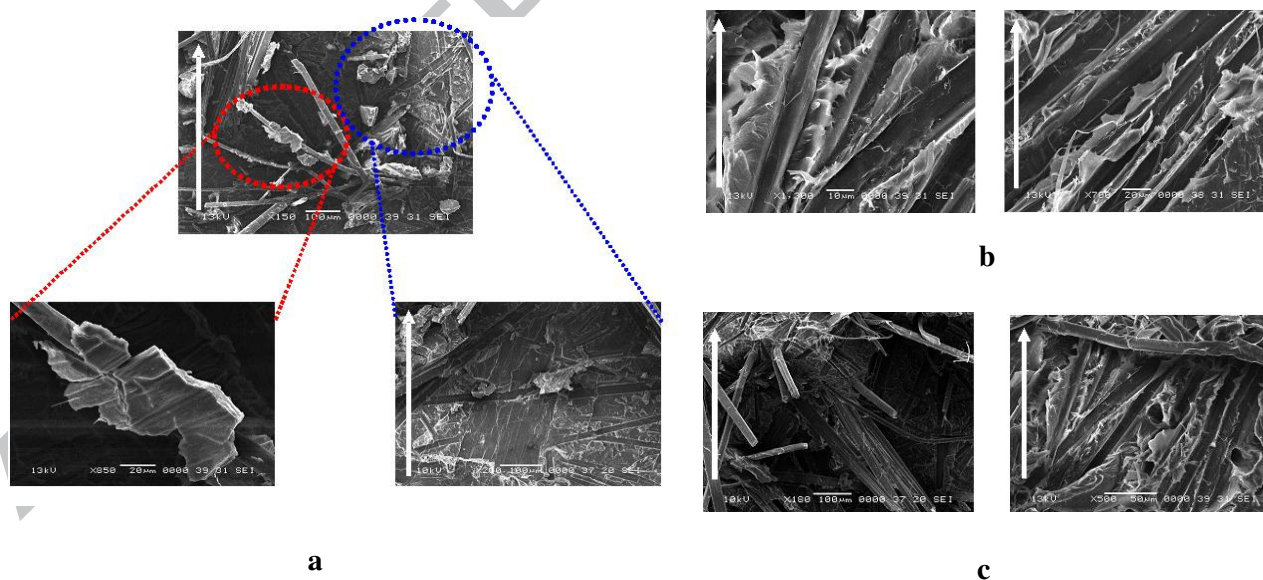


Fig. 10 SEM photo of slow cooled mode I specimen a) 1.5°C/min., white arrows indicate delamination direction.

b) Sample cooled at 15.5°C c) fast cooled (93°C/min) mode I fracture surfaces

Table Captions

Table 1 Thermal properties (DSC) for different cooling rates

Table 2 Mechanical properties in tension and shear of PLLA for different thermal conditions [4]. Mean values \pm standard deviations

Table 3 Critical stress intensity factor (K_{Ic}), and fracture energy (G_{Ic}) of PLLA for different manufacturing conditions. Mean values \pm standard deviations

Table 4 In-plane shear properties of Flax/PLLA bio-composite for different thermal conditions. Mean values \pm standard deviations

Table 5 Measured and estimated in-plane shear modulus of Flax/PLLA biocomposites.

Table 6 Critical strain energy release rates at initiation G_{Ic} . Mean values \pm standard deviations

Table 7 Energy balance for mode I cracking

Table 1 Thermal properties (DSC) for different cooling rates

Material	Thermal treatment	ΔH_c (J/g)	ΔH_m (J/g)	Degree of crystallinity (%)
PLLA	93°C/min	25.8	26	-
	Annealing	24.9	25.3	-
	15.5°C/min	23	26.7	8
	1.5°C/min	1.6	37.7	33

Table 2 Mechanical properties and their standard deviation in tension and shear of PLLA for different thermal conditions [4]

Material	Thermal treatment	Tension			Shear	
		E (MPa)	σ_r (MPa)	ϵ_r %	G_{12} (MPa)	τ_{12} (MPa)
PLLA	93°C/min	3029 ± 410	56 ± 1	1.7 ± 0.3	1303 ± 476	33 ± 0.6
	Annealing	3394 ± 149	58.3 ± 3	1.8 ± 0.2	1463 ± 120	33.7 ± 1.7
	15.5°C/min	3743 ± 368	60.9 ± 3.2	2.2 ± 0.1	1609 ± 144	35.2 ± 1.8
	1.5°C/min	4003 ± 410	64.4 ± 1	0.6 ± 0.2	1743 ± 176	37.8 ± 3.3

Table 3 Critical stress intensity factor (K_{Ic}), fracture energy (G_{Ic}) and their standard deviation of PLLA for different manufacturing conditions.

Material	Thermal treatment	K_{Ic} (MPa.m ^{1/2})	G_{Ic} (J/m ²)
PLLA	93°C/min	1.66 ± 0.28	433 ± 73
	Annealing	1.96 ± 0.30	512 ± 79
	15.5°C/min	2.08 ± 0.34	544 ± 90
	1.5°C/min	0.63 ± 0.02	165 ± 49

Table 4 In-plane shear properties and their standard deviation of Flax/PLLA bio-composite for different thermal conditions

Material	Cooling rate (°C/min)	Composite		PLLA	
		G ₁₂ (MPa)	τ ₁₂ (MPa)	G ₁₂ (MPa)	τ ₁₂ (MPa)
Flax/PLLA	93	1989 ± 159	22.6 ± 3.1	1303 ± 476	33 ± 0.6
	annealing	1972 ± 89	21.1 ± 1.4	1463 ± 120	33.7 ± 1.7
	15.5	2308 ± 74	33.9 ± 2.1	1609 ± 144	35.2 ± 1.8
	1.5	1776 ± 252	18.5 ± 1.1	1743 ± 176	37.8 ± 3.3

Table 5 Measured and estimated in-plane shear modulus of Flax/PLLA biocomposites.

Material	Cooling rate (°C/min)	G ₁₂ measured (MPa)	G ₁₂ calculated with Eq. 5 (MPa)	Difference (%)
Flax/PLLA	93	1989 ± 159	1704	-14.4
	annealed	1972 ± 89	1859	- 5.8
	15.5	2308 ± 74	1994	- 13.7
	1.5	1776 ± 252	2115	+19.1

Table 6 Critical strain energy release rate and their standard deviation at initiation G_{Ic}

Treatment	n	$G_{Ic, onset} (J/m^2)$	Coefficient of variation (%)
93°C/min	2.43	191 ± 58	30
Annealing	2.55	184 ± 67	36
15.6°C/min	2.29	323 ± 43	13
1.5°C/min	2.15	65 ± 15	24

Thermal treatment	G_{Ic} matrix (J/m ²)	G_{Ic} interface (J/m ²) [4]	G_{Ic} composite initiation measured (J/m ²)	G_{Ic} calculated composite hexagonal (Eq. 14)	Difference (%)	G_{Ic} calculated composite square (Eq.17)	Difference (%)
93°C/min or air*	433 ± 73	29 ± 17	191 ± 58	216	+13	200	+5
Annealing	512 ± 79	13 ± 2	184 ± 67	245	+33	225	+22
15.6°C/min or 10°C/min*	544 ± 90	33 ± 14	323 ± 43	270	-16	250	-33
1.5°C/min or 1°C/min*	165 ± 49	41 ± 17	65 ± 15	99	+53	94	+45

Table 7 Energy balance for mode I cracking